

## **IN THE SPECIFICATION**

Please amend the specification as follows:

Please replace the paragraph beginning at page 14, line 24 through page 15, line 8 with the following rewritten paragraph:

-- More specifically, the delivery pressures of the hydraulic pumps 1, 2 and the control pressure from the solenoid control valve 32 are introduced respectively to pressure bearing chambers 22a, 22b and 22c of the second servo valve 22. When the sum of hydraulic forces of the delivery pressures of the hydraulic pumps 1, 2 is smaller than a setting value that is determined depending on a difference between the force of a spring 22d and the hydraulic force of the control pressure introduced to the pressure bearing chamber 22c, a valve member 22e is moved to the right, as viewed in Fig. 1, whereupon the large-diameter pressure bearing chamber 20d of the tilting actuator 20 is communicated with the reservoir 12 via the return fluid line 13 to increase the tilting of the hydraulic pump 1 or 2. As the sum of hydraulic forces of the delivery pressures of the hydraulic pumps 1, 2 increases in excess of the above-mentioned setting value, the valve member ~~22a~~22e is moved to the left, as viewed in Fig. 1, whereupon the pilot pressure from the pilot pump 9 is transmitted to the pressure bearing chamber 20d to decrease the tilting of the hydraulic pump 1 or 2. Further, when the control pressure from the solenoid control valve 32 is low, the above-mentioned setting value is increased so that the tilting of the hydraulic pump 1 or 2 starts to decrease from a relatively high delivery pressure of the hydraulic pump 1 or 2. As the control pressure from the solenoid control valve 32 rises, the above-

mentioned setting value is reduced so that the tilting of the hydraulic pump 1 or 2 starts to decrease from a lower delivery pressure of the hydraulic pump 1 or 2.--

Please replace the paragraph beginning at page 19, line 24 through page 20, line 15 with the following paragraph:

-- The engine load increase amount computing unit 70f, the engine revolution speed increase gain computing unit 70g, the multiplier 70h, the engine revolution speed increment value selector 70i, the primary delay element 70j, the subtracter 70k, the subtracter 70m, the gain multiplier 70n, the integral adder 70p, and the primary delay element 70q constitute a means 90 (hereinafter referred to as a "revolution speed modification value computing unit") for computing the increase amount of the engine revolution speed, as a revolution speed modification value  $\Delta T3$ , based on respective change rates of the control pilot pressures PP1, PP2, the pump tiltings SR1, SR2, and the pump delivery pressures DP1, DP2, which are status variables related to the loads of the hydraulic pumps 1, 2. The modification value adder 70r adds the revolution speed modification value  $\Delta T3$  to the target engine revolution speed NR1 applied from the input unit 71, and then inputs the resulting sum, as a target engine revolution speed NR2 for use in the control, to the base torque computing unit ~~70f~~70s. These points will be described in more detail below.--

Please replace the paragraph beginning at page 22, line 21 through page 23, line 10 with the following rewritten paragraph:

-- The engine revolution speed increment value selector 70i determines whether the determination value  $\alpha$  is positive, negative or 0, and it switches over an engine revolution speed increment value  $\Delta T2A$ , which is applied to the subtracter 70m, depending on the determination result. If  $\alpha \geq 0$  (namely if the engine revolution speed increase amount  $\Delta T2$  is changed in the increasing direction, or if  $\Delta T2$  is not changed), the selector 70i is held in a state B to select the engine revolution speed increase amount  $\Delta T2$  so that the engine revolution speed increase amount  $\Delta T2$  is outputted as the increment value  $\Delta T2A$  applied to the subtracter 70m. If  $\alpha < 0$  (namely if the engine revolution speed increase amount  $\Delta T2$  is changed in the decreasing direction), the selector 70i takes a state A to select 0 as the increment value  $\Delta T2A$  applied to the subtracter 70m. At the time of switching from the state B to A, the operation is delayed for a certain time (e.g., 3 seconds) to provide the hold function of maintaining the previous value.--

Please replace the paragraph beginning at page 23, line 16 and ending at line 21 with the following paragraph:

-- The gain multiplier 70n serves to give the deviation  $\Delta \Delta T2$  a primary delay. A primary delay gain is set to 1 when the deviation  $\Delta \Delta T2$  is in the increasing direction (i.e.,  $\Delta \Delta T2 \geq 0$ ), and to a value smaller than 1 when the deviation  $\Delta \Delta T2$  is in the

decreasing direction (i.e.,  $\Delta\Delta T2 < 0$ ). The gain is multiplied by  $\Delta\Delta T2$  to obtain a deviation  $\Delta\Delta T4$ .--

Please replace the paragraph beginning at page 28, line 5 and ending at line 11 with the following paragraph:

-- During this period, since the control lever is quickly manipulated, the load increase amount  $\Delta T1$  is computed as a value other than 0 in the engine load increase amount computing unit 70f, and the multiplier 70h multiplies the load increase amount  $\Delta T1$  by the engine revolution speed increase amount  $\Delta T2$  depending on the target revolution speed NR1 at that time.--

Please replace the paragraph beginning at page 28, line 5, and ending at line 11 with the following paragraph:

-- During this period, since the control lever is quickly manipulated, the load increase amount  $\Delta T1$  is computed as a value other than 0 in the engine load increase amount computing unit 70f, and the multiplier 70h multiplies the load increase amount  $\Delta T1$  by the gain  $K\Delta T1$  ~~the engine revolution speed increase amount  $\Delta T2$~~  depending on the target revolution speed NR1 at that time to compute the engine revolution speed increase amount  $\Delta T2$ .--